



```

QN3      VNPN  VN      0      NPNV  1
QN4      VN    VN      0      NPNV  1
RN1      VCC   VN1     5K
RN2      VCC   VN2     5K

VCC      VCC    0       12
VREF     VREF   0       6
IPNP     VP     0       20u
INPN     VCC   VN      20u

BDITA    VIOUT  0       I = ( V(VP2) - V(VP1) + V(VN2) - V(VN1) )/5000
BOTA     OUT    0       I = -1*( V(VIOUT) - V(VREF) )/50
CCOMP    OUT    VIOUT  20p

.tran    100n   50u     0      100n

.model   NPNV  npn  BF=150
.model   PNPV  pnp  BF=150

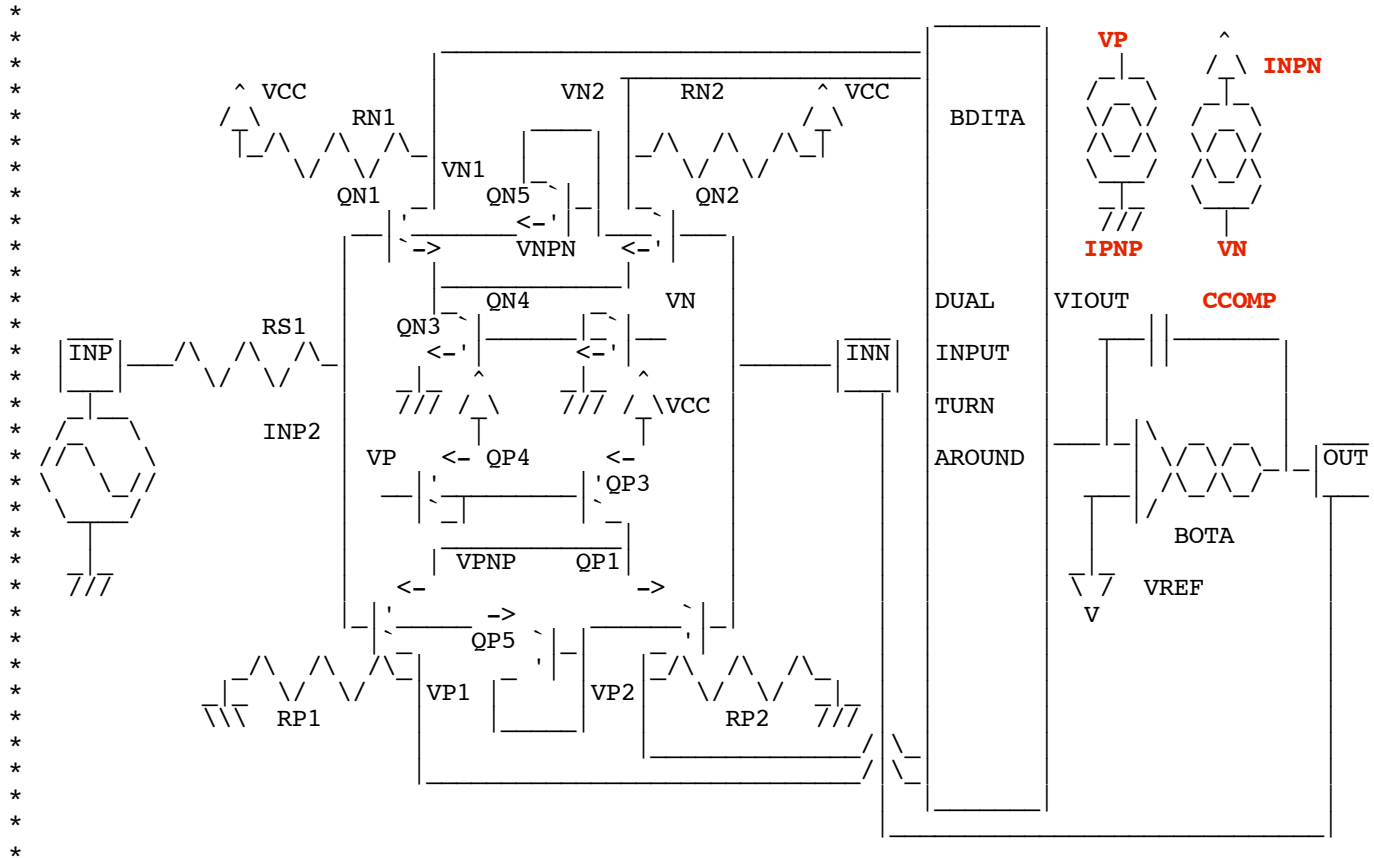
.control
run
set      pensize = 2
plot    v(out) v(inp)
.endc
.end

```

\* =====END=====

To Covert PDF to plain text click below  
<http://www.fileformat.info/convert/doc/pdf2txt.htm>

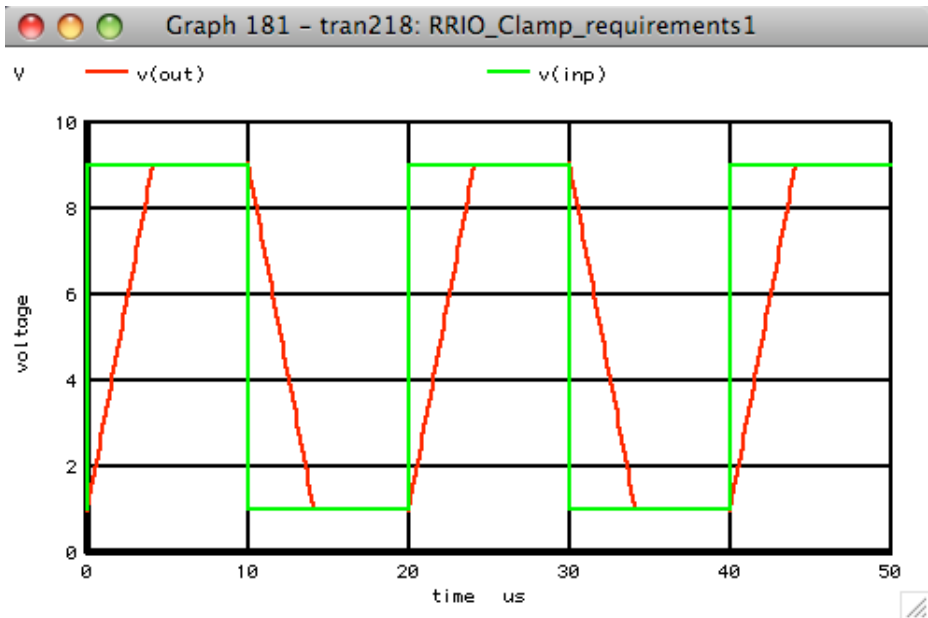
The development of vertical pnps was a natural for RRIO Op Amp Design. The vertical pnps are about a thousand times faster and have at least ten times better beta than lateral pnps.



For the LM6142, the tail currents IPNP of the input stages was chosen by weighing an input bias current spec against a process beta spec. That chosen, the desired GainBandWidth for the Op Amp defines the magnitude of the compensation capacitor CCOMP used. This in turn

defines the slew of the Op amp which is simply +/- full tail current into the compensation capacitor CCOMP.

Connecting the Op Amp up as a simple voltage follower demonstrates why the input clamp diodes are needed. Both vertical npns and pnps will be destroyed with reverse emitter base voltages above a few volts. Just supplying a square wave to a voltage follower application will do that because the output of the Op Amp may not be able to slew as fast as the input signal.



In the case of this simulation, current limiting resistor RS1 and clamp diodes QN5 and QP5 keep the voltages across the input transistors to within reason during the slewing period.