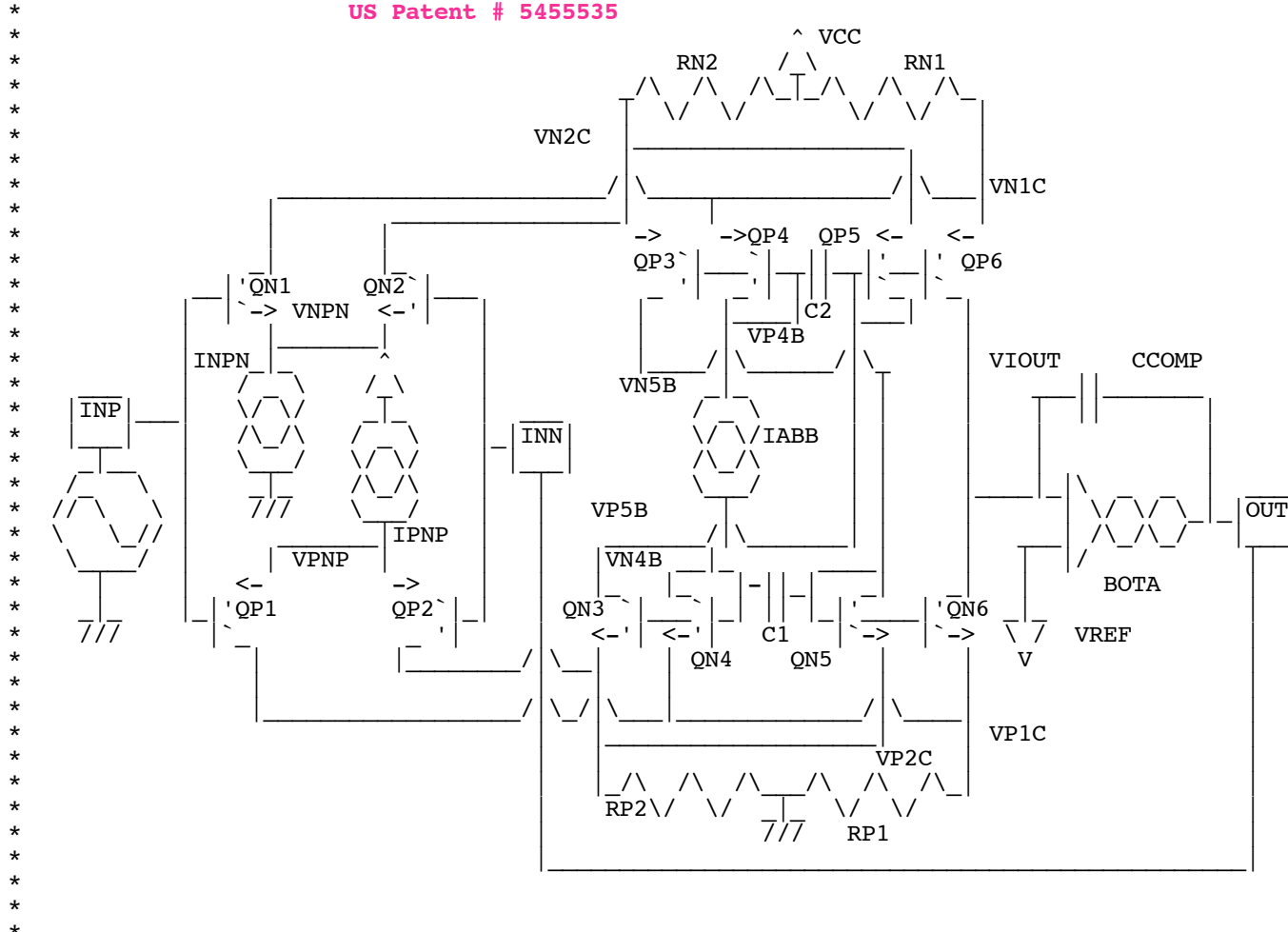


GAIN_HALFER

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US Patent # 5455535



.OPTIONS method=trap

| | | | | | | |
|-----|------|------|------|------|----|----|
| VIN | INP | 0 | DC | 6 | AC | 1m |
| QP1 | VP1C | INP | VPNP | PNPV | 1 | |
| QP2 | VP2C | OUT | VPNP | PNPV | 1 | |
| RP1 | VP1C | 0 | 5K | | | |
| RP2 | VP2C | 0 | 5K | | | |
| QN1 | VN1C | INP | VNPN | NPNV | 1 | |
| QN2 | VN2C | OUT | VNPN | NPNV | 1 | |
| RN1 | VCC | VN1C | 5K | | | |
| RN2 | VCC | VN2C | 5K | | | |

```

VCC      VCC      0      12
VREF     VREF     0      6
IPNP     VCC      VPNP   20u
INPN     VNPN     0      20n

QP3      VN5B     VP4B2   VN2C     PNPV    1
RP3      VP4B2    VP4B     1000
QP4      VP4B     VP4B     VN1C     PNPV    1
QP5      VP5B     VP5B     VN2C     PNPV    1
RP5      VP5B2    VP5B     1000
QP6      VIOUT    VP5B2    VN1C     PNPV    1

QN3      VP5B     VN4B2    VP2C     NPNV    1
RN3      VN4B2    VN4B     1000
QN4      VN4B     VN4B     VP1C     NPNV    1
QN5      VN5B     VN5B     VP2C     NPNV    1
RN5      VN5B2    VN5B     1000
QN6      VIOUT    VN5B2    VP1C     NPNV    1

IABB     VP4B     VN4B     5u
BOTA     OUT     0      I = -1*( V(VIOUT) - V(VREF) )/1
CCOMP    OUT     VIOUT    1p

C2       VP4B2    VP5B2    3f
C1       VN4B2    VN5B2    3f

.model1  NPNV    npn      BF=150   CJE=.6p  CJC=.3p  CJS=1p
.model1  PNPV    pnp      BF=60    CJE=.6p  CJC=.3p  CJS=1p

.control
run

ac       dec    10    10k    100000K
set      pensize = 2
let      gain = v(out)/( v(out)- v(inp) )
plot     dB(gain ) phase(gain) title Without_Halfer

alter    C1  capacitance = 3p
alter    C2  capacitance = 3p
ac       dec    10    10k    100000K
set      pensize = 2
let      gain = v(out)/( v(out)- v(inp) )
plot     dB(gain ) phase(gain) title With_Halfer

.endc
.end

* =====END=====

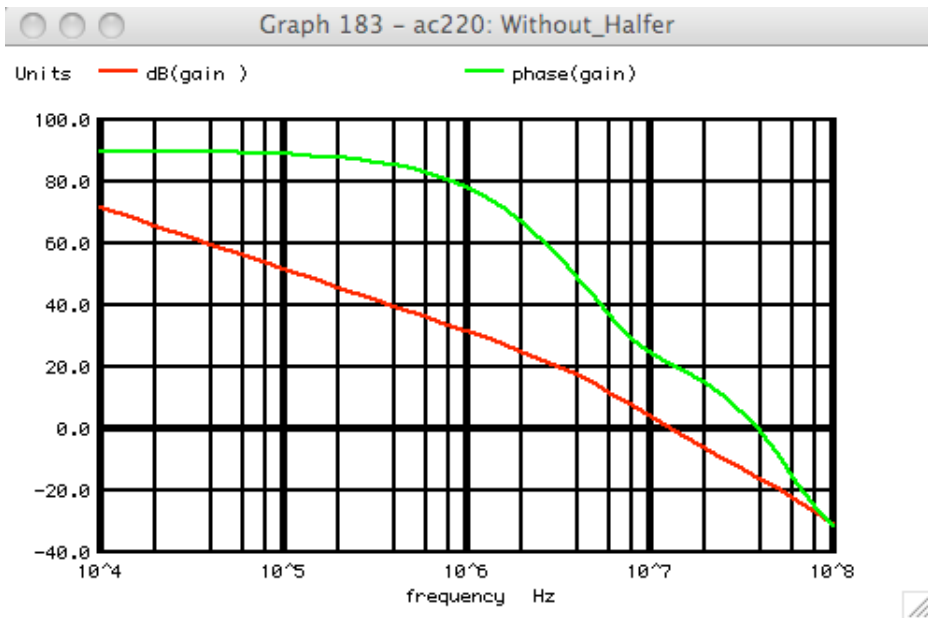
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<http://www.fileformat.info/convert/doc/pdf2txt.htm>

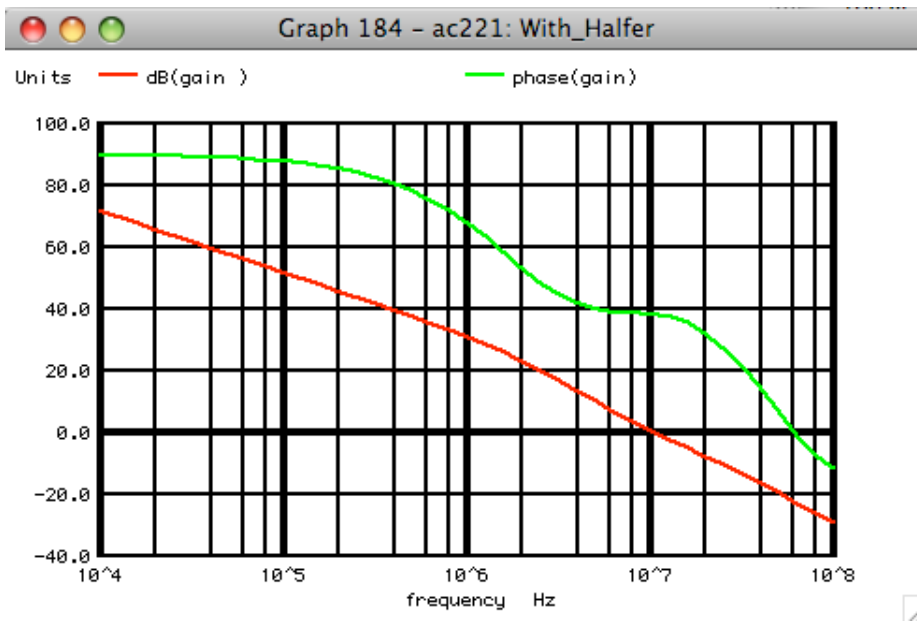
The LM6142 is a current starved design. The idea was to design a 10MHz unity gain stable Op Amp which drew less than 1mA per amplifier using a process very close to the standard analog process.

The main challenge was the size of transistors. The process was a 30volt process. The dimensions were such that stray capacitance was in terms of pico farads instead of femto farads.

Perhaps the dominate challenge was the emitter base stray capacitance which was around 0.5pF. A transistor will have a junction impedance of 26Kohm at 1uA of emitter current. That puts f_{tau} at 10MHz. The problem is that a large number of such transistors running minimum current need to be put into the signal path. Each transistor contributes time delay to the signal and the goal is to have the total overall time delay small enough that there is less than 180 of phase shift at 10MHz in order for the Op Amp to be unity gain stable.



The simulation above is looking at the phase shift due to the dual input turn around just modeling stray capacitance. The unity gain cross is around 15Mhz. At that frequency there may be a little more than 20degrees of phase margin.



The result is a bit counter intuitive looking at the resulting gain phase plot. Both gain and phase delay are reduced at higher frequencies. For a normal lowpass, a gain decrease normally results in a phase delay increase. What is happening in the circuit is half of the dual turn around's signal path which has the most transistors and therefore the most delay has been removed at the higher frequencies. This is the "shorten the signal path" technique.